Doppler Wind profiler uncertainty in a turbulent atmosphere

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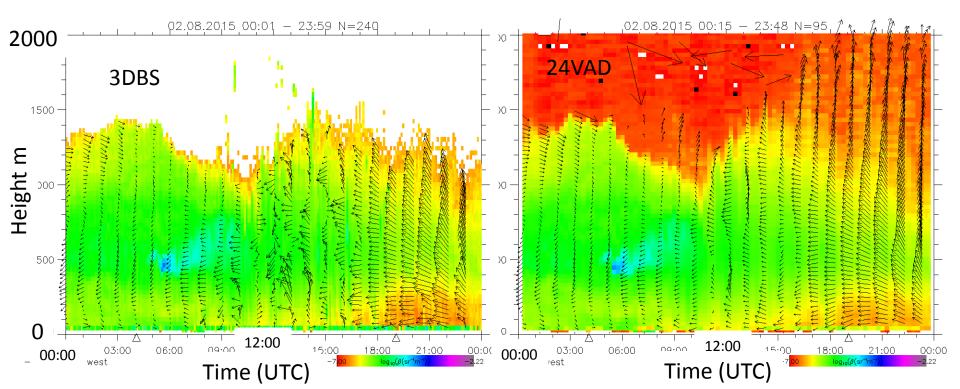
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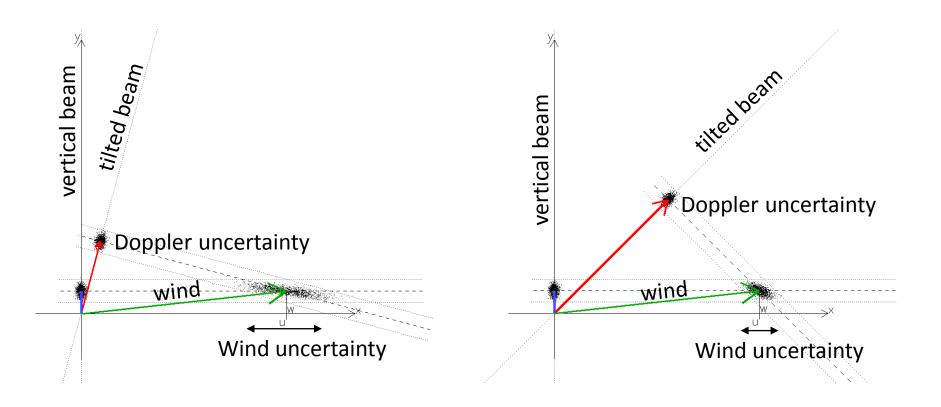
Motivation

- More and more Doppler wind profiler available (radar, sodar, lidar) -> e-prof
- providing wind data to assimilation requires uncertainty estimates
- Current uncertainty estimate consider only Doppler uncertainty – not turbulence



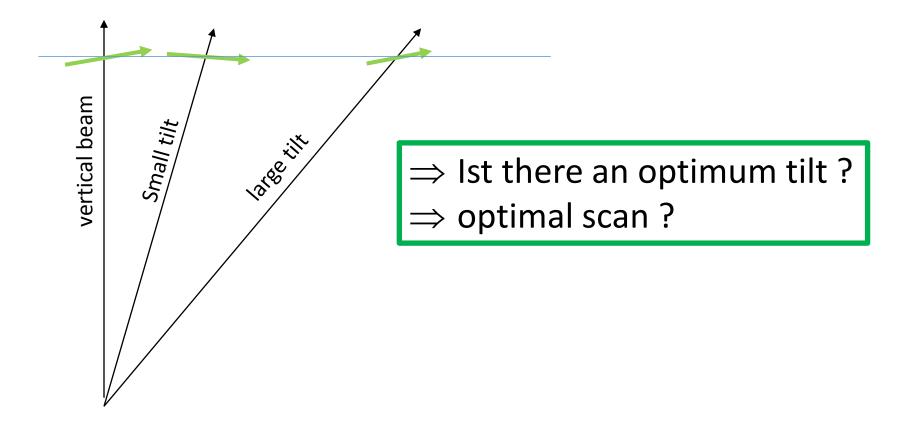
Motivation: large tilt

- To get horizontal wind component beams must be tilted
- The larger the tilt the smaller the uncertainty
- => tilt should be large !



Motivation: small tilt

- Large tilt => large separation => different wind
- Tilt should be small !



Two beams + turbulence

- One vertical and one tilted beam
- Differences in wind speeds due to separation
- Gaussian error propagation
- Separation introduces auto- and cross-covariances between *u,u and u,w* etc. at the two locations of the vertical beam (r₁) and the tilted beam (r₂):
 - If there is upwind at r_1 there might be also upwind at r_2 => $C_{ww}(r_1, r_2) = \overline{w'_{r1}w_{r2}}' / \overline{w'_{r1}}'^2$
 - If there is upwind at r_1 horizontal wind speed at r_1 might be lower

$$=>C_{uw}(r_1, r_2) = \overline{u'_{r1}w'_{r2}} / \overline{u'_{r1}w'_{r1}}$$

• .

assumptions

homogeneity of the turbulent field

$$\Rightarrow \dots \quad \overline{u_{s1}^{\prime 2}} = \overline{u_{s0}^{\prime 2}} = \overline{u^{\prime 2}} \text{ and } \overline{u_{s1}^{\prime} w_{s1}^{\prime}} = \overline{u_{s0}^{\prime} w_{s0}^{\prime}} = \overline{u^{\prime} w^{\prime}}$$

- horizontal isotropy for form of C_{uu}, C_{uw} etc.
 => depend only on scalar distance
- All normalized auto- and cross-covariances are the **same**:

$$C_{uu}(r) = C_{uw}(r) = C(r)$$

• Especially the last is a very strong assumption. But we believe deviations are small enough to allow for the use in this *uncertainty estimate*

Two beams: equation

• Equation for one vertical one tilted beam

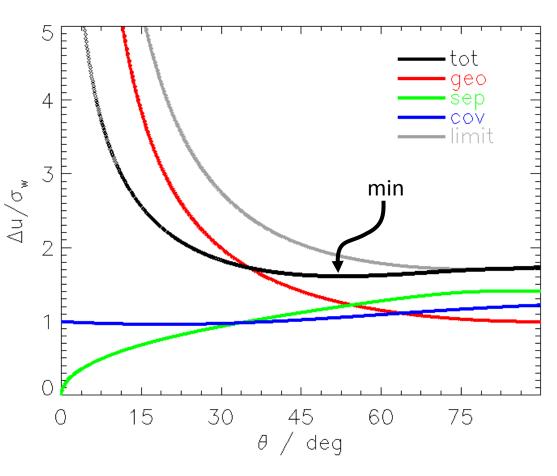
$$\left(\frac{\Delta u_{rs}}{\sigma_w}\right)^2 = \frac{1}{s_\theta^2} \cdot 2\left[1 - C(r_{01})\right] \cdot \left(s_\theta^2 \cdot \frac{\overline{u'^2}}{\sigma_w^2} + 2s_\theta c_\theta \cdot \frac{\overline{u'w'}}{\sigma_w^2} + c_\theta^2\right)$$
separation
Geometry
Effect of (co-)variances

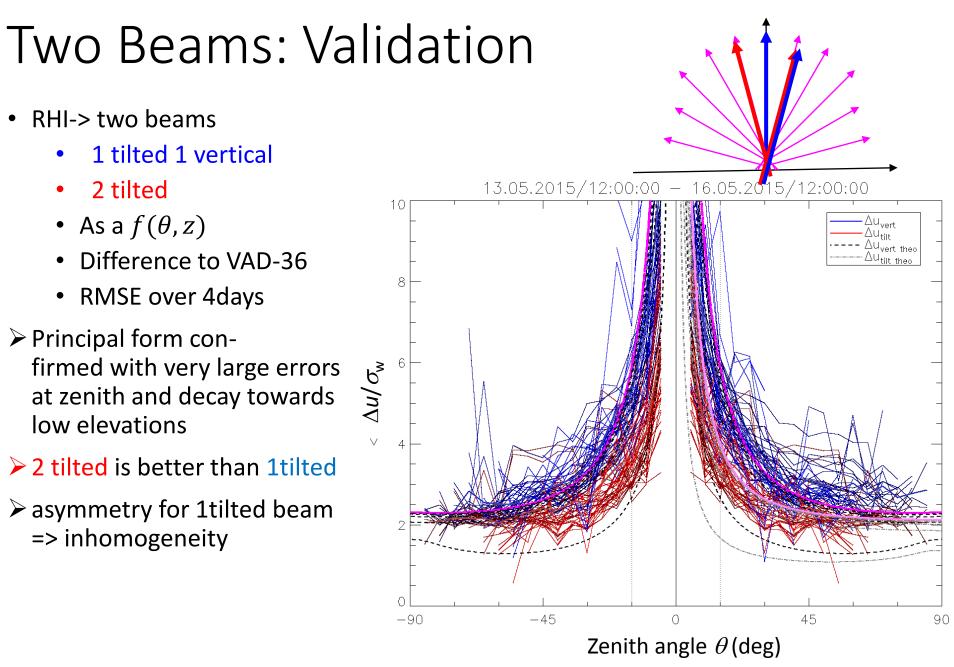
$$s_{\theta} = \sin \theta, c_{\theta} = \cos \theta$$

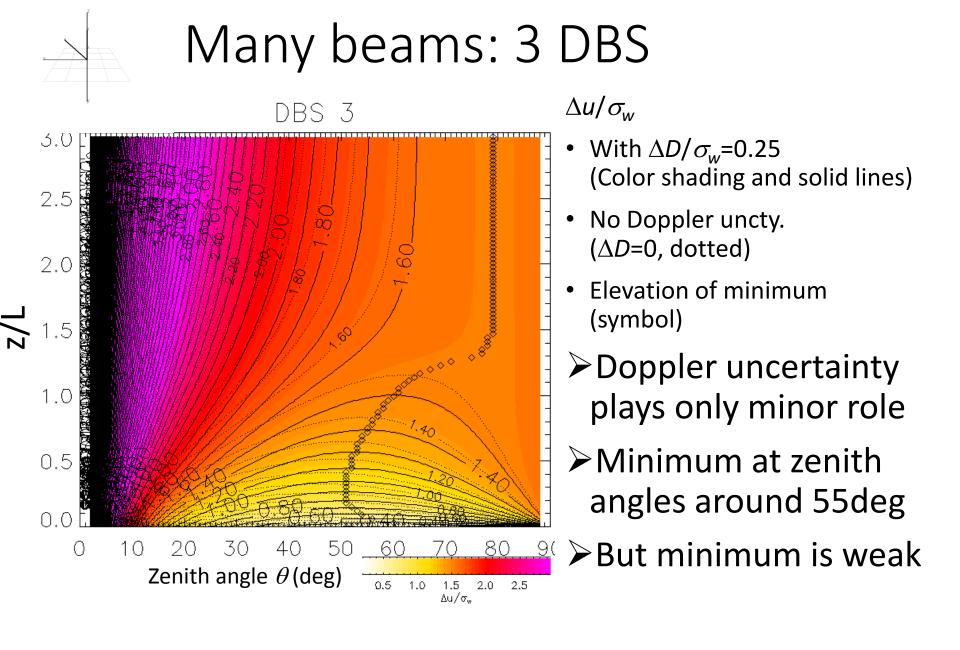
• Similar equations can be derived for any arbitrary scan pattern

Two Beams:

- $C(r)=\exp(-r/L)$ $r = z \cdot \tan \theta$, z = L = 300m, $uu/\sigma_w^2=1.2$, $uw/\sigma_w^2=-0.2$
- geometry factor dominates
- Efect of (co-)variances is small => we do not need to know uw etc. exactly
- ≻Weak Minimum at ~50deg
- uncertainty of 2-tilted beams is smaller than 1tilt+1vertical

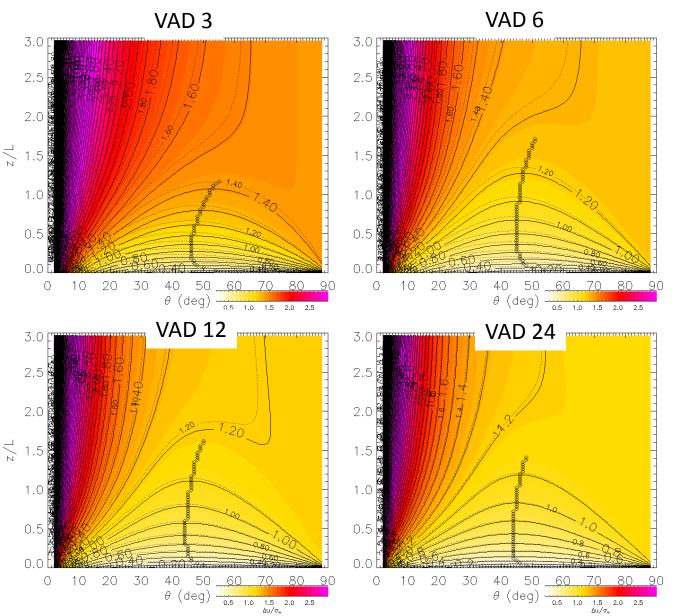






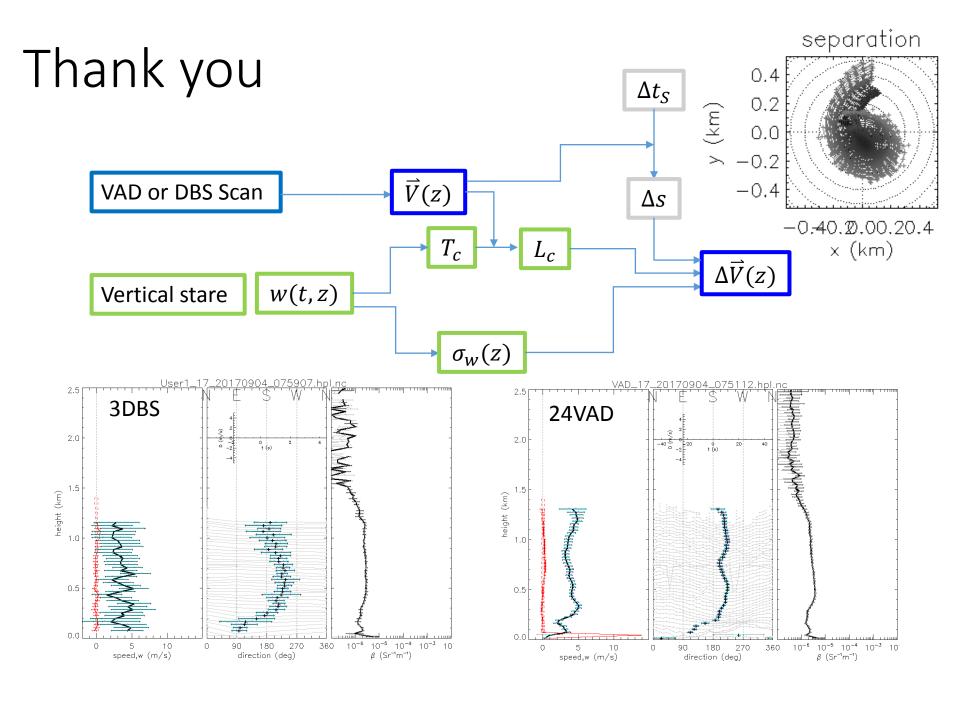
Many beams: ...

- Increasing the number of beams reduces uncertainty but follows not $1/\sqrt{N}$ law
- Minimum remains at +/- the same place and stays weak
- Larger zenith angle decreases uncty.
 but effect diminishes above ~30deg.



Conclusions

- Uncertrainty estimate requires knowledge of
 - covariance matrix of the wind,
 - spatial auto- and cross-correlations of the wind components
 - we solved this with simplifiactions/assumptions
- DBS-3 scan has larger uncertainty than VAD-3
- More beams decrease uncertainty
 - but effect is less than $1/\sqrt{N}$ law and
 - diminishes with increasing N
 - gain for N>12 is minimal
- Uncertainty decreases with increasing zenith angles
 - effect is for θ >30° small
 - there is a weak minimum around 55deg at low heights.



Acknowledgments: COST-TOPROF, ET-CC (German Excellence initiative Cologne), Guy Pearson, ...